

ASSESSMENT OF WIND-INDUCED RESPONSES OF STRUCTURES USING WIND TUNNEL TESTING

VLERESIMI I SJELLJES SE STRUKTURAVE NDAJ NGARKESAVE TE ERES NEPERMJET TESTIMIT NE TUNELET E ERES

Redefining possible.

Bujar Morava, Ph.D., P.Eng., M.ASCE Senior Technical Director / Principal RWDI CANADA



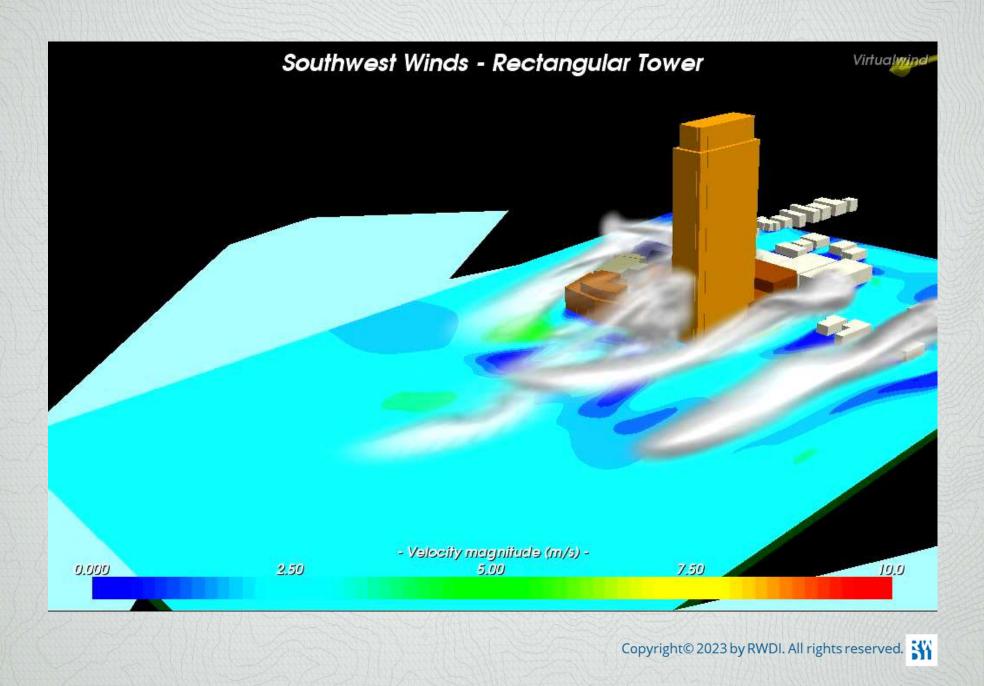
- Code-based procedures for assessment of wind loading
- The need for wind tunnel testing
- Wind tunnel modeling techniques and methodologies
- Assessment of wind-induced motion comfort
- Aerodynamic shape optimization
- Supplemental damping system implementation

Widely Recognized Code-Based Analytical Procedures for Assessment of Wind Loading

ASCE 7-16 Standard, Sections 26 – 30

- National Building Code of Canada (NBCC 2015), Section 4.1.7.
- Australian/New Zealand Standard AS/NZS 1170.2:2021, Part 2: Wind Actions.
- Eurocode 1 Actions on Structures, Part 1-4, General Actions – Wind Actions

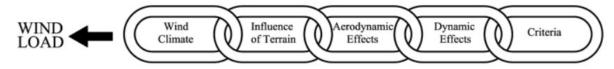
Wind & Structures - How do they interact?



How is this complex interaction represented in the ASCE 7 and other code wind load calculation procedures?

Southwest Winds - Rectangular Tower Virtualwir p = f(Kz, Kzt, Kd, V, I, Gf, Cp)

THE ALAN G. DAVENPORT WIND LOADING CHAIN



Definition of Coefficients Used in the ASCE 7-16 Wind Load Calculation Procedure

- \succ K_z wind exposure category factor.
- ➤ K_{z,t} topographic effects factor
- K_d wind directionality factor
- \succ V_b basic wind speed for the proposed site
- I building importance or building risk category factor used to determine V_b for the proposed site
- \succ G_f gust effect factor
- C_p building aerodynamic shape factor

Note: It is important to keep in mind that the averaging time used in the definition of basic wind speed V_b is different from code to code.

Averaging Times Used in the Definition of Basic Wind Speeds of Different Codes

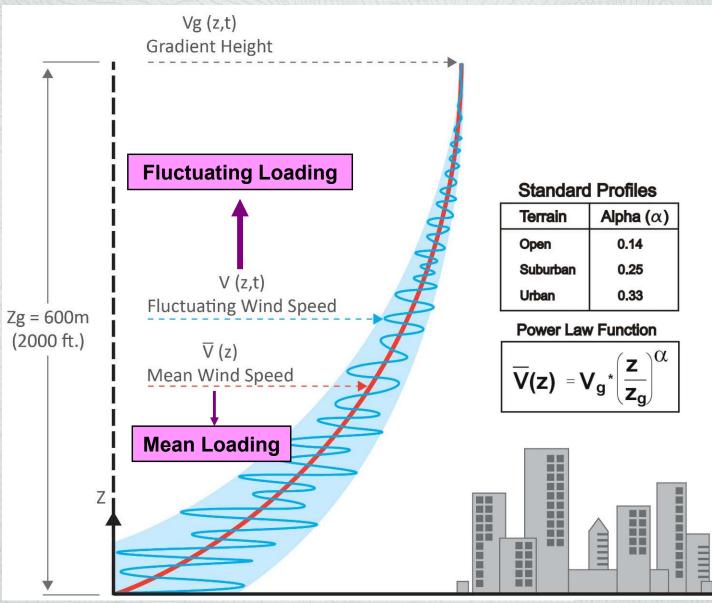
Code or Standard Name	Averaging Time Used in the Definition of $\rm V_b$	
ASCE 7-16	3-seconds	
NBCC 2015	1-hour	
AS/NZS 1170.2:2021	3-seconds	
EUROCODE 1	10-minutes	

Conversion Factors to Convert the V_b from One Averaging Time or Code to Another

From - To	From - To	Conversion Factor
10-minutes to 1-hour	EUROCODE 1 to NBCC 2015	0.939
10-minutes to 3-seconds	EUROCODE 1 TO ASCE 7-16 EUROCODE 1 TO AS/NZS 1170.2:2021	1.432

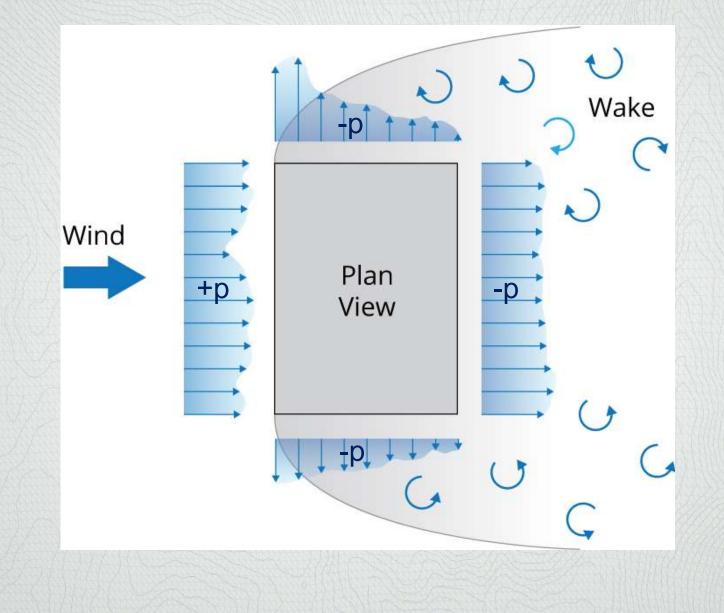
Example: If it is desired to run wind loading calculations for a high-rise building in Tirana using NBCC 2015 or ASCE -16 procedure, then the corresponding mean hourly and 3-sec gust basic wind speeds applicable for NBCC 2015 and ASCE 7-16 will be 30 x 0.939 = 28.2 m/s and 30 x 1.432 = 43 m/s, respectively.

How Does Wind Speed Vary with Height?

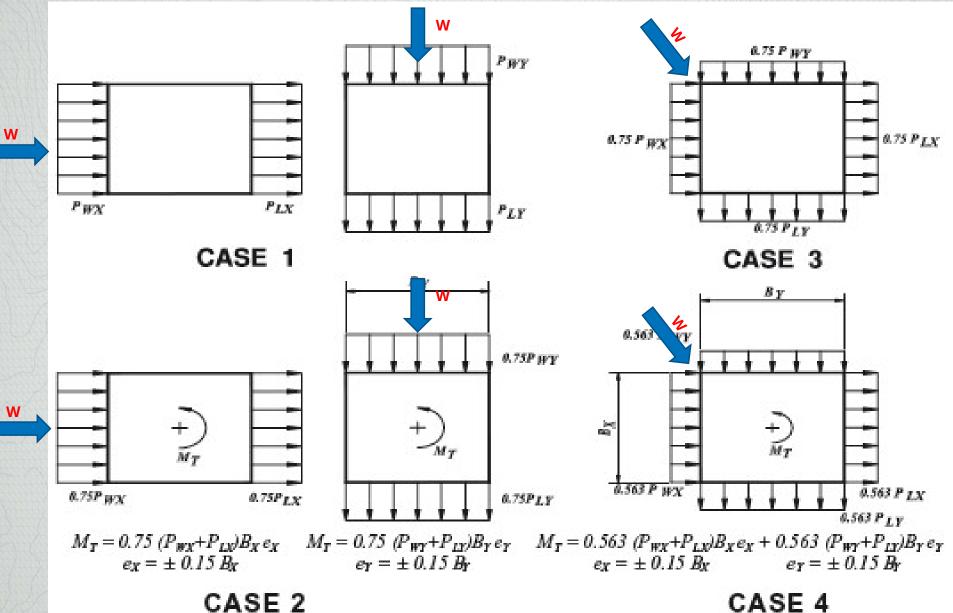


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Instantaneous Pressure Distribution Around a Building



How is the Simultaneous Action of Wind Pressures Around a Building Considered in ASCE 7 Procedures?



CASE 2

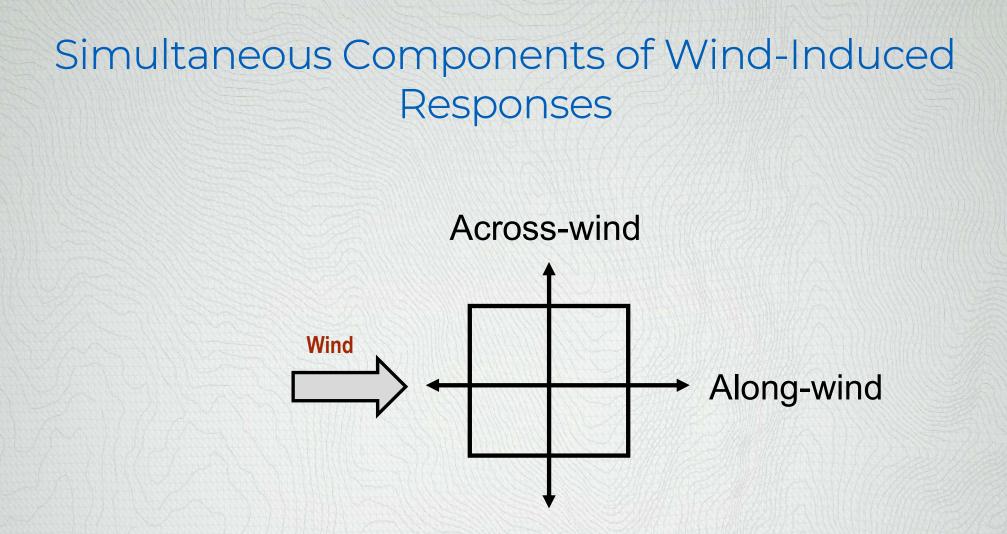
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The ASCE 7 wind load calculation procedure applicability and limitations

1. The building *is a regular-shaped* building or structure as defined in Section 26.2.

2. The building *does not have* response characteristics making it subject to across wind loading, vortex shedding, instability due to galloping or flutter; or does not have a site location for which <u>channeling effects or buffeting in the wake of upwind obstructions warrant special consideration.</u>

LIMITATIONS: Buildings or other structures not meeting the above requirements or *having unusual shapes* or response characteristics, shall be designed using recognized literature documenting such wind load effects or shall *use the wind tunnel procedure* specified in Chapter 31.



Along-wind => addressed by code analytical procedures

Across-wind => NOT addressed by code procedures!!

Across-wind vibrations are usually greater than along-wind vibrations for buildings of heights greater than 120m

Illustration of Simultaneous Components of Wind-Induced Responses

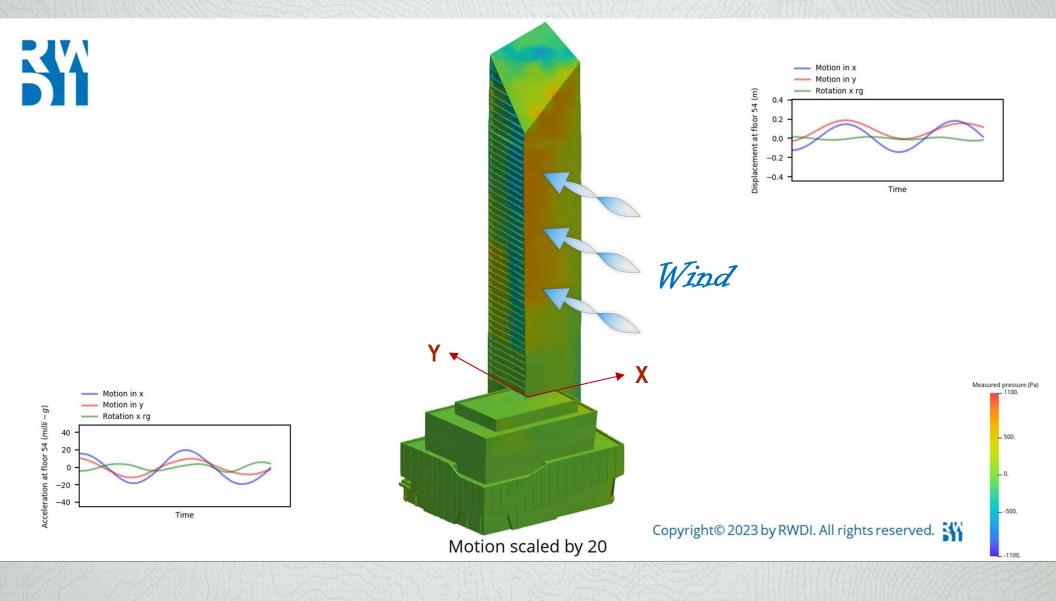
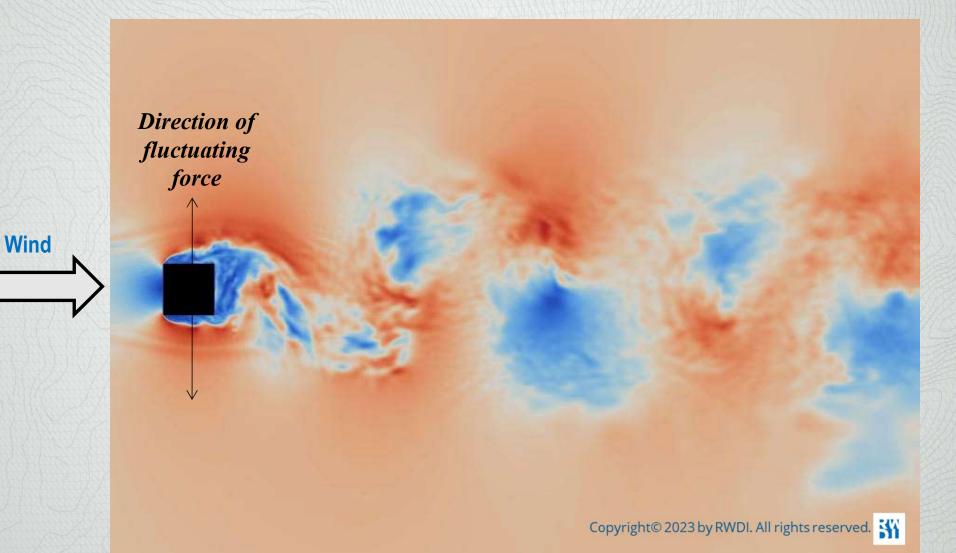


Illustration of Across-Wind Response in a Square Section



Why would we conduct an experiment to determine wind loads?

Wind loads may be difficult to predict because:

- Complexity of building shapes
- Interference effects from neighboring buildings
- Complexity of upwind terrain
- Dynamic behavior under wind action
- Lack of resolution provided by building codes and standards

Building Shapes non Compliant with Code

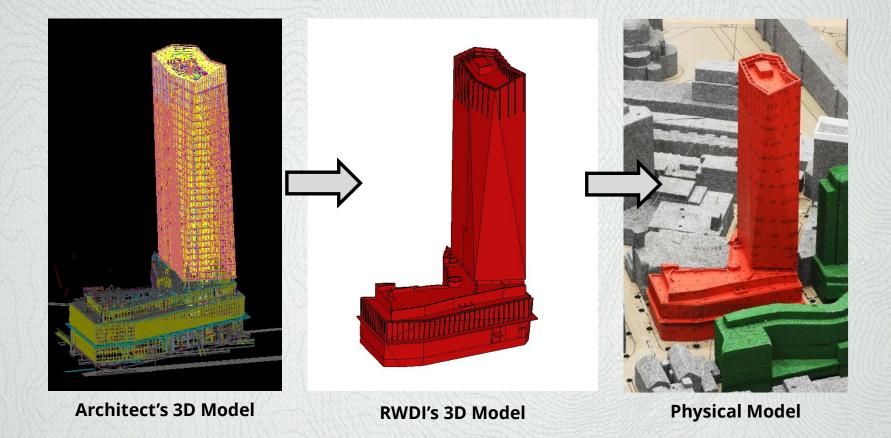


Building Shapes non Compliant with Code





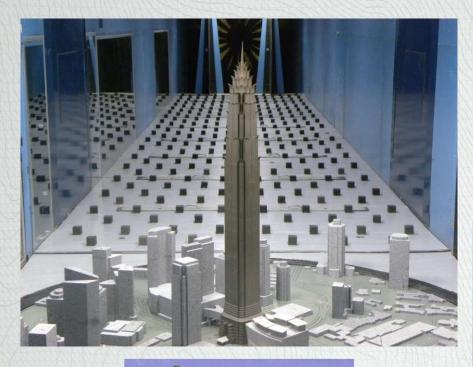
Wind Tunnel Study Model



Wind Tunnel Study Types Conducted for Buildings and Other Structures

- Structural wind load studies
 - Buildings
 - Long span roof
 - Complex shape structures
- Cladding wind load studies
 - Buildings
 - Long-span roof
 - Complex shape structures
- Aeroelastic wind response studies
 - Tall, slender buildings
 - Bridges
 - Spires and other dynamically sensitive structures

Wind Tunnel Modeling and Testing Techniques Used for Buildings and Other Structures







High-Frequency-Force-Balance (HFFB) Copyright© 2023 by RWDI. All rights reserved.

Wind Tunnel Modeling and Testing Techniques Used for Buildings and Other Structures



Generalized Wind Force Using HFPI

$$F_{Gx}(t) = \sum_{i} \sum_{j} p_{ij}(t) \phi_{xi} A_{ij} \cos \alpha_{ij}$$

p_{ij} = pressure on tributary area A_{ii} Normal to tributary areaA_{ii} x = direction

of modal



Level i

Location j-1

Level (i-1)

Tributary Area A_{ii} deflection ϕ_{γ}

Location i+1

Location j

High-Frequency-Pressure-Integration (HFPI)

The First High-Rise Buildings of Albania Evaluated Through Wind Tunnel Modeling and Testing

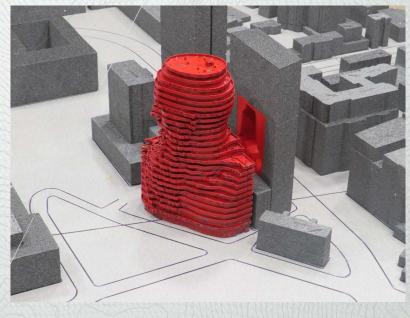




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Downtown One Tirana Tower



Tirana's Rock

RWDI's Wind Tunnel Testing Facilities



Atmospheric Boundary Layer Simulation Wind Profile Development

Illustration of Wind Tunnel Simulation of Wind Profiles



Far-field simulation of effective overall wind conditions using spires

Near-field simulation using proximity model

and floor roughness



Summary of Steps Involved in a Detailed Wind Tunnel Study

- Assess surrounding terrain (i.e. wind exposure/profile) at the project site
- Evaluate the local wind climate
- Construct a physical model
- Test the model in the wind tunnel
- Record and process the data, combine them with the dynamic properties of the structure (i.e. frequencies, masses, mode shapes & damping)
- > Integrate the results with the local wind climate
- Summarize/Interpret results in a user-friendly format

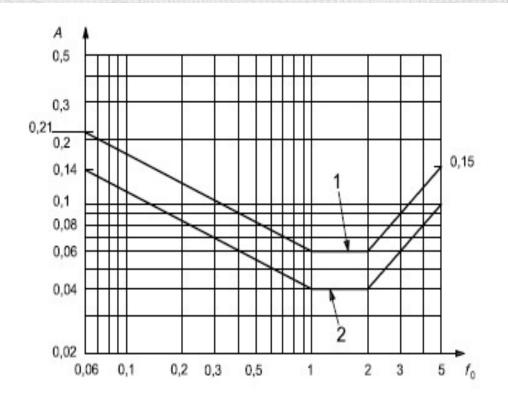
Commonly Used Wind-Induced Motion Comfort Criteria (10-year return period wind events)

Building Type	10-Year Peak Acceleration in milli - g	
Residential	15 - 18	
Hotel	18 - 20	
Office	20 - 25	

Note: 1-milli-g = 1/1000 of gravity acceleration

ISO Wind-Induced Motion Comfort Criteria

1-year return period wind events Frequency dependence



Key

.4 peak acceleration, m/s²

f₀ first natural frequency in a structural direction of a building and in torsion, Hz

1 offices

2 residences

Figure D.1 — Evaluation curves for wind-induced vibrations in buildings in a horizontal (x, y) direction for a one-year return period

RWDI Suggested Torsional Velocity Criteria*

Peak torsional velocity at the top occupied floor of the building should be at or below the following values:		HAR SALE AND THE AND T	Acceptable hourly peak values of Torsional Velocities	
		1-year RP event	10-year event	
		(milli-rad/sec)	(milli-rad/sec)	
	Residential Occupancy	2.0	4.0	
-	Office Occupancy	2.5	5.0	

* Based on RWDI's experience including motion simulator experiments.

What are the factors affecting windinduced responses of structures?

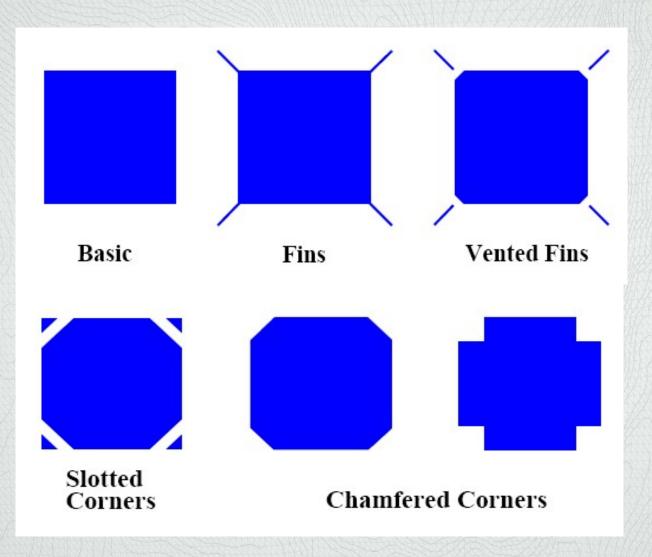
Wind Speed and Direction
Aerodynamic Shape

Structural Stiffness - K

> Mass - M

> Damping - ξ

Aerodynamic Modifications

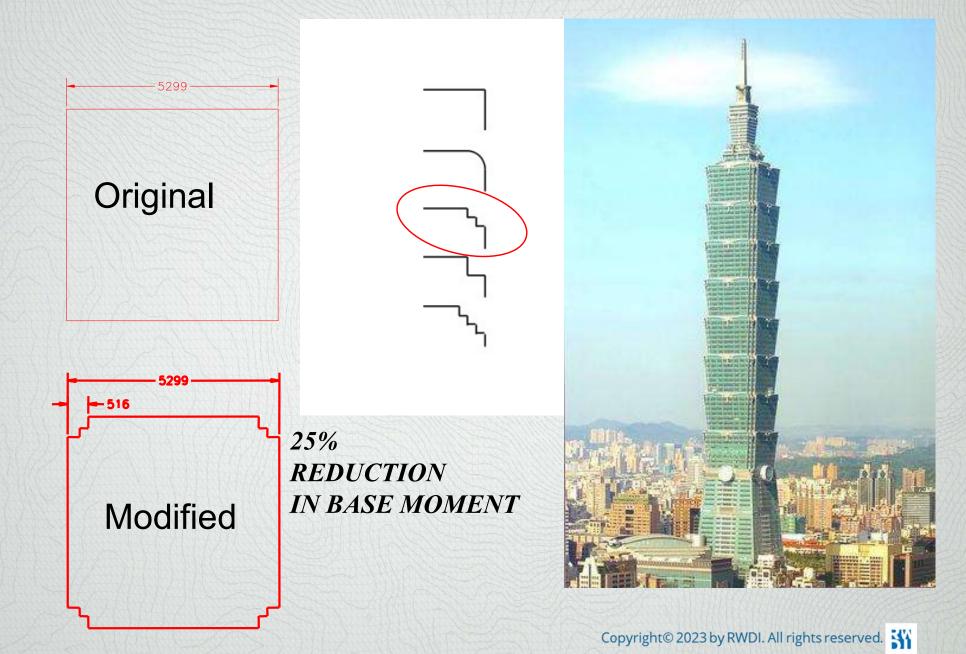


Taipei 101 Aerodynamic Modification Effects

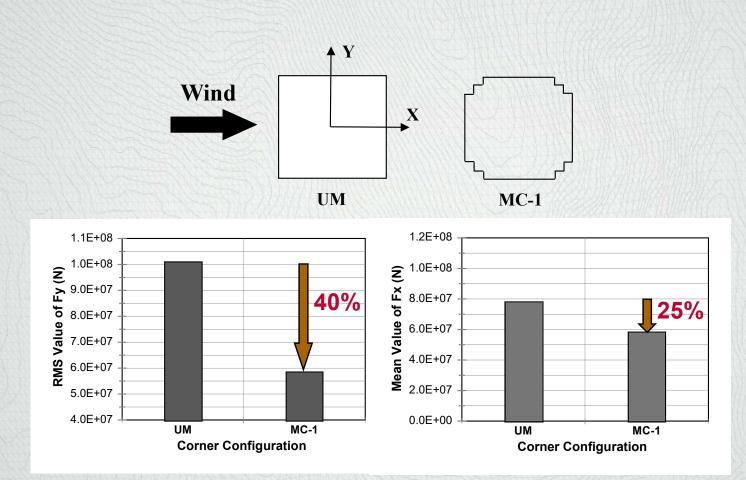


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Taipei 101 Tower Original and Modified cross-sections

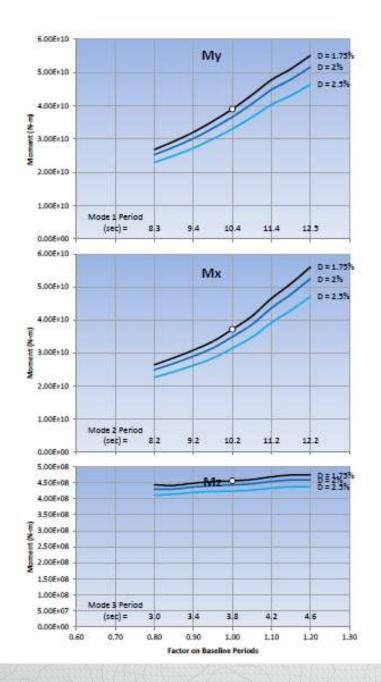


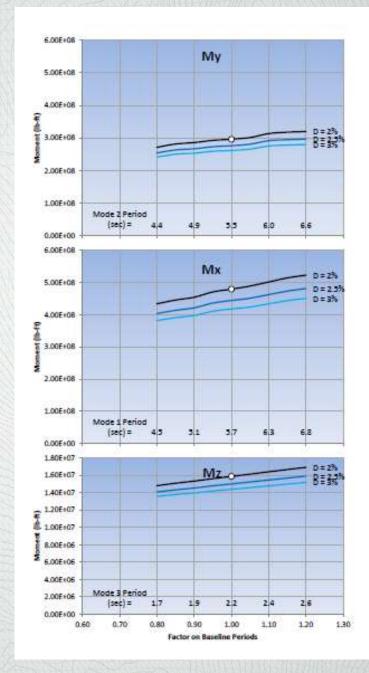
Reduction of Wind-Induced Responses



Aerodynamic Modification Effects

Structural Dynamic Optimization

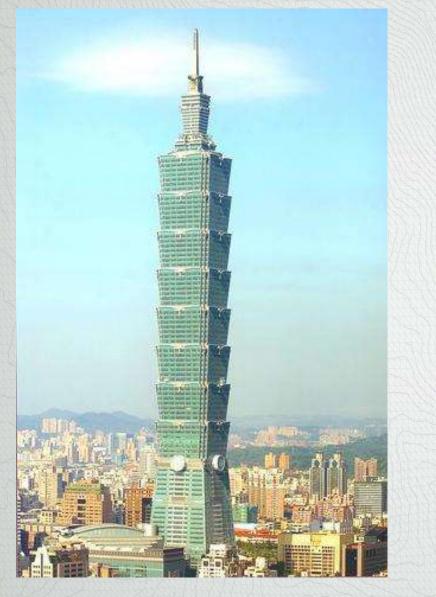


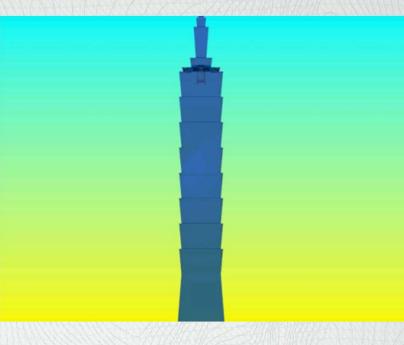


Building A – Overall Wind Loading at Base

Building B – Overall Wind Loading at Base

Supplemental Damping System Implementation







Tuned Mass Dampers (TMD) – Taipei 101 Tower – Taipei - Taiwan

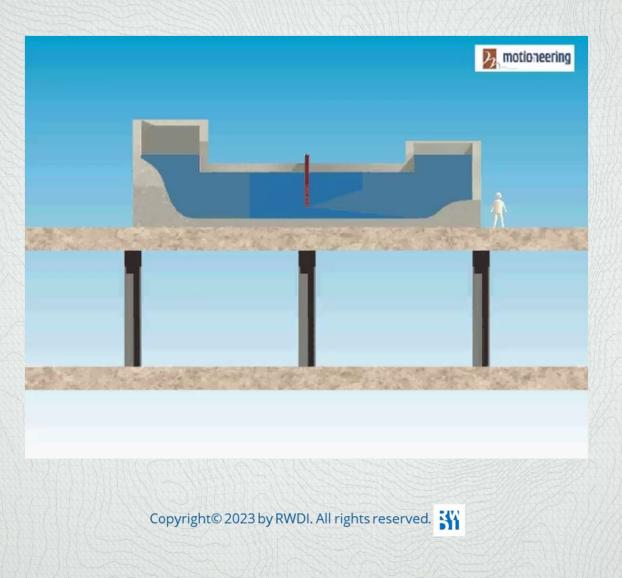
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Supplemental Damping System Implementation



Tuned Sloshing Damper (TSD)

Supplemental Damping System Implementation



Tuned Liquid Column Damper (TLCD)



THANK YOU

Redefining possible.